

Metallographic preparation of High Alloy Tool Steels

Steels can broadly be classified into three categories based on chemical composition:

- Carbon steels
- Low alloy steels with small amounts of alloying elements
- High alloy steels with >6% alloying elements

In addition to carbon, high alloy steels contain large amounts of alloying elements such as chromium, nickel, vanadium, tungsten and molybdenum. Wear resistance, toughness, strength and hardness are the most important characteristics of tool steel, and the alloying elements mentioned improve and optimize these mechanical properties, and, if added in sufficient amounts, provide specific properties such as corrosion and heat resistance, retention of hardness at high temperatures, and retention of strength at low temperatures etc.

The increasing demands of advanced production technologies and economic pressures in all industries require steel manufacturers to constantly improve the quality of high performance tool steel alloys for special and demanding applications. For example, steels for making punches, dies or cutting tools require very specific properties such as high strength and hardness combined with toughness. In addition, these steels require

a high standard of cleanliness. Such properties can only be achieved by carefully controlling all stages of steelmaking, and subsequent forging/rolling and heat treatment processes.

The main demands on the metallography departments of steel producers of high quality alloyed tool steels are the following:

- To handle high sample volumes efficiently,
- To use, if possible, one standard procedure for all steel qualities,
- And to deliver well polished surfaces with undamaged carbides and inclusions.

This is particularly important for evaluating structures with carbides and inclusions of ultra clean steel.

The metallographic sample evaluation includes distribution and size of carbides, detection of decarburization of hardened and then tempered steels, detection of micro-segregations and inclusion ratings.



*Cold work tool steel.
Tool for punching*



Plastic mould steel etched with 5% Picral, revealing some singular needles and plates at high magnification in an otherwise amorphous martensite

1000x, DIC

Difficulties during metallographic preparation

Cutting:

Efficient cutting without overheating.



Fig. 1: Thermal damage due to faulty cutting conditions

Grinding and polishing: Handling large sample volumes. Very fine carbides and inclusions can be pulled out of the soft matrix; large carbides can be cracked during plane grinding.



Fig. 2: Fractured primary carbides

200x

Solution:

- Selecting the correct cut-off wheel
- Using automatic grinding and polishing equipment
- Sufficient diamond polishing to polish past the mechanical damage of grinding

Production and application

The production process of high alloy steels is a sophisticated process of melting and remelting. A mixture of iron and well sorted scrap is first melted in an electric arc furnace, and cast into an ingot form, or continuously cast into bloom or billet. For many applications these primary products can be further processed into bar, rod or plate form. For steels with higher quality demands, the primary product can be used as feedstock for a secondary steelmaking process. This secondary process can be a double or even triple remelt by vacuum induction melting plus vacuum arc remelting, or electroslag remelting, which can also be done under pressure and protective gases.

The main purpose of this secondary process is to reduce impurities such as oxides, sulphides and silicates so that with successive remelts the degree of cleanliness increases and homogenous ingots with excellent mechanical and physical properties are produced. The high cost of these energy intensive remelting techniques is reflected in the price of high temperature and corrosion resistant martensitic and hot work tool steels for special applications.

The range of high alloy steels is very wide and some products are even tailor-made for especially demanding applications. Following are some examples of high alloy tool steels and their applications, with the approximate content of main alloying elements:

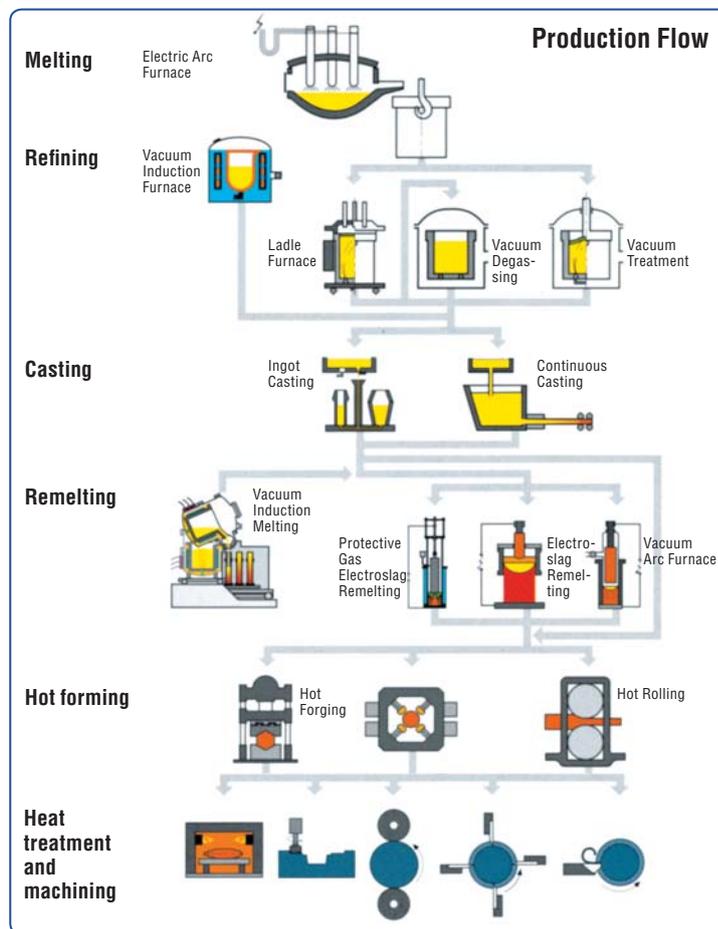


Fig. 3: Production flow for high alloy tool steels

Cold work tool steel: 1.6-2% carbon, 5-12% chromium, for punching, stamping, deep drawing, thread rolling tools, shear blades.

Properties: high toughness, high compressive strength and wear resistance, good nitrideability.

Hot work tool steel: 0.38% carbon, 5% chromium, 1.5-3% molybdenum and 0.5% vanadium, for pressure die casting tools.

Properties: high hot strength, toughness and wear resistance, high thermal fatigue and shock resistance.

High speed tool steels: 0.75-1.3% carbon, 4.5% chromium, 2% vanadium, 6-18% tungsten, 4-9% molybdenum, for taps, turning and milling tools.

Properties: retention of hardness and toughness at elevated temperature.

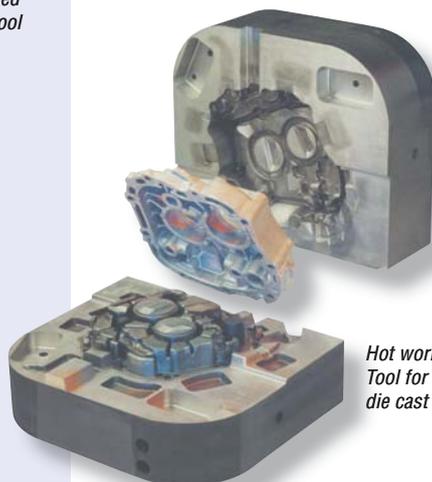
Plastic mould steel: 0.3% carbon, 12-17% chromium, for molding plastic parts for the automotive, medical and consumer goods industry.

Properties: Can be polished to high surface finish, exceptional toughness and hardness, good corrosion resistance.

For tool making the steel is used in the as tempered condition. After the tool is machined it is surface hardened by nitriding or induction hardening. The conditions under which tools have to operate are varied and sometimes extreme. Therefore, the variations in alloys for tool steels are very wide in order to accommodate the best possible selection for specific difficult and demanding tool applications.



High speed cutting tool



Hot work tool steel. Tool for pressure die cast



Tool for moulding plastic

Difficulties in the preparation of high alloy tool steels

As heat treatability of tool steels is a quality criterion, thermal influence during cutting has to be avoided in order to give a true representation of the actual structure. When cutting larger sections and failure analysis samples this preparation step has to be carried out with great care.

The main difficulty of grinding and polishing high alloyed tool steels is the retention of carbides and non metallic inclusions. In cold working tool steels primary carbides are very large and fracture easily during grinding. In the fully annealed conditions, secondary carbides are very fine and can easily be pulled out from the softer matrix. (See Fig. 2 front page, micrograph with cracked carbides).

Processing large sample volumes of different high alloy tool steels during various stages of the production can be a challenge, which requires a very efficient organisation of the workflow, automatic equipment and standard procedures.



Recommendations for the preparation of high alloyed steels

Cutting

The majority of samples are usually sectioned by rough mechanical means from slabs and blooming mill material into standard sizes. Critical cuts for heat treatment samples or failure analysis are always carried out with a metallographic cut-off machine. High alloy tool steels are extremely sensitive to thermal damage. Therefore special care must be taken to select the appropriate cut-off wheels and secure sufficient cooling for cutting. Soft aluminium oxide or resin bonded cubic boron nitride cut-off wheels are recommended.



Mounting

Depending on the size and volume of the samples and the information that is needed from them, the specimens can be unmounted, hot or cold mounted. Surface treated samples that need good edge retention should be hot compression mounted using fibre-reinforced resins (IsoFast, DuroFast). Samples that do not require edge retention can be left unmounted if their dimensions are suited for sample holders. For standardizing sample sizes, which can be an advantage when handling large volumes, cold mounting in rectangular silicon or polypropylene mold cups (UnoForm) is recommended. It is important that the cold mounting resin has little shrinkage to avoid contamination due to gaps between sample and resin.

Grinding and polishing

The main requirements on the preparation of high alloy tool steels are a true representation of form, amount and size of carbides, and the retention of non-metallic inclusions in an undeformed matrix. Large volumes of samples of



high alloy steels are best processed on fully automatic grinding and polishing machines, which guarantee a

fast and efficient workflow and reproducible results. As tool steels are hard, fine grinding with diamond is more efficient and economical than grinding with silicon carbide paper. Sometimes a final oxide polish after the diamond polishing step can be useful for contrasting and identifying carbides.

Following are suggestions for preparation methods with fully automatic grinding and polishing equipment, and semi-automatic equipment respectively.

These methods are based on experience and offer excellent reproducible results. Small changes may have to be made to accommodate specific requirements or personal preferences.



Grinding			
Step	PG	FG	
Surface	Stone 150#	MD-Allegro	
Suspension		9 µm	
Lubricant	Water	Blue	
rpm	1450	150	
Force [N]	300	300	
Time	As needed	9 min.	

Polishing			
Step	DP 1	DP 2	
Surface	MD-Dac	MD-Nap	
Suspension	6 µm	1 µm	
Lubricant	Blue	Blue	
rpm	150	150	
Force [N]	300	150	
Time	6 min.	4 min.	

Table 1: Preparation method for high alloy tool steel on large automatic equipment

The preparation data in Table 1 are for 6 samples, 65x30 mm, unmounted or cold mounted, using Struers MAPS or AbraPlan/AbraPol.

For smaller sizes and numbers of samples semi-automatic grinding and polishing equipment will give also good, reproducible results.

The data in Table 2 are for 6 samples, 30 mm mounted, clamped into a sample holder, using Struers TegraPol-31/ TegraForce-3 with TegraDoser-5.

Grinding			
Step	PG	FG	
Surface	MD-Piano 220	MD-Allegro	
Suspension		DiaPro Allegro/Largo	
Lubricant	Water		
rpm	300	150	
Force [N]	210	210	
Time	As needed	9 min.	

Polishing				
Step	DP 1	DP 2	OP 1*	
Surface	MD-Dac	MD-Nap	MD-Chem	
Suspension	DiaPro Dac	DiaPro Nap B	OP-AA	
rpm	150	150	150	
Force [N]	210	150	90	
Time	6 min.	1 min.	1 min.	

Remark: DiaPro diamond suspensions can be substituted with DP-Diamond suspension P as follows: For FG with 9µm, DP 1 with 3 µm, DP 2 with 1µm.

*Optional

Table 2: Preparation method for high alloy tool steel on table models semi-automatic equipment

Etching and structure interpretation

Etching

Usually samples of tool steel are first examined unetched to identify inclusions and carbide size and formation.

For revealing the structure, either Nital or picric acid in various concentrations is used. For instance, to show the carbide distribution in cold work steel a 10% Nital colors the matrix dark while

the white primary carbides stand out. For fine globular pearlite a brief submersion into picric acid followed by 2% Nital gives a good contrast and avoids staining.

For mixing and working with etching solutions standard safety precautions have to be observed.



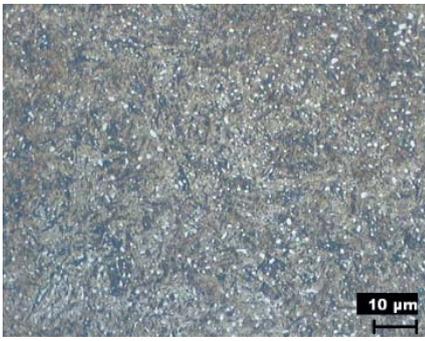
Fig. 4: Cold work tool steel etched with 10% Nital, primary carbides stand out white

100x



Fig. 5: Hot work tool steel etched with Picral and Nital, globular pearlite

500x



High speed tool steel after final heat treatment, very fine structured martensite with chromium carbides

Nital:

100 ml ethanol

2-10 ml nitric acid (*Caution do not exceed 10% solution, explosive!*)

Picric acid etching solution:

100 ml ethanol

1-5 ml hydrochloric acid

1-4 g picric acid

Structure interpretation

Generally high alloyed steels have the same structural phases as regular iron-carbon alloys: ferrite, pearlite, martensite and austenite, but the solid solution can absorb a certain amount of alloying elements. Carbon forms complex carbides with some alloying elements such as chromium, tungsten and vanadium. In addition, the solubility of carbon in iron changes: Adding alloying elements such as silicon, chromium, tungsten, molybdenum and vanadium increases the alpha area of the iron-iron carbon diagram, while adding nickel and manganese will enlarge the gamma area. These characteristics influence the time-temperature transformation which is specifically important for the heat treatment of tool steels.

The primary structure of cold work tool steel is a ledeburite. Its coarse structure is transformed through hot rolling or forging into a ferritic-pearlitic matrix with large primary carbides (Fig. 6). A subsequent full annealing shapes the secondary fine carbides (Fig. 7).

Hot work tool steels in the fully heat treated condition show ideally a tempered martensitic matrix containing very fine globular pearlite (Fig. 5). Here it is important that segregations from the primary structure are as much as possible evened out through heat treatment as uneven chemical composition can lead to corrosion problems (Fig. 8).

Plastic mould steel is a corrosion resistant tool steel which before heat treating shows an “amorphous” martensite with strings of carbides (Fig. 9). After annealing it shows finely dispersed carbides (Fig. 10).

The even distribution of carbides in tool steel can be improved by powder metallurgical process. Through a powder making process and subsequent hot isostatic pressing, a homogenous, segregation free steel is made, which is especially suitable for unconventional tool geometries that would be expensive to make by mechanical means (Figs. 11 and 12).



Fig. 6: Cold work tool steel after initial hot forming, slightly contrasted by a short final oxide polish, showing large primary carbides in a ferritic-pearlitic matrix 200x

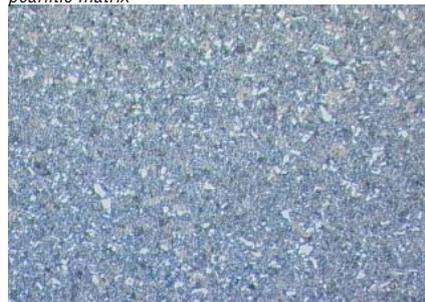


Fig. 7: Fully heat treated cold work tool steel showing very finely dispersed secondary carbides and small white primary carbides 200x



Fig. 8: Hot work tool steel showing segregations 100x

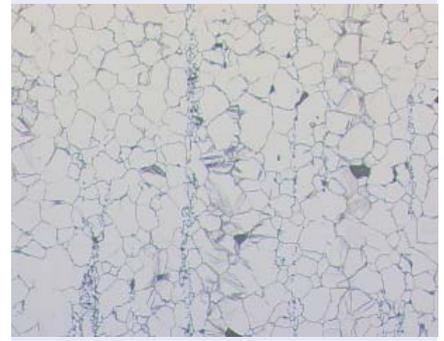


Fig. 9: Plastic mould steel, etched in 5% Picral, amorphous martensite with strings of primary carbides 100x



Fig. 10: Plastic mould steel after annealing shows very fine carbides 500x



Fig. 11: Carbide distribution in conventionally produced steel



Fig. 12: Carbide distribution in powder metallurgically produced steel

Struers A/S
 Pederstrupvej 84
 DK-2750 Ballerup, Denmark
 Phone +45 44 600 800
 Fax +45 44 600 801
 struers@struers.dk



Summary

An ever larger portion of high alloy tool steels are today made to fit customers' applications. This requires the production of very clean material with very specific mechanical, physical and metallurgical properties. Metallographic inspection from the initial casting and first forming stages, to the final semi-finished, heat treated product, is an essential tool for controlling manufacturing and heat treatment processes.

The main challenges regarding metallographic preparation are managing the large sample volume, and producing consistently excellent surface finishes. As size, form and distribution of carbides and inclusion are the main quality indicators of tool steel, it is essential that they are retained during preparation. Automatic grinding and polishing, using diamond for fine grinding and polishing, gives good and reproducible results. Using one preparation method applicable for all the various types of tools steels makes the handling easy and efficient.

Application Notes

Metallographic preparation of High Alloy Tool Steels

Elisabeth Weidmann, Anne Guesnier, Struers A/S, Copenhagen
 Judy Arner, Struers Inc, Westlake, Ohio, USA
 Bill Taylor, Struers, Ltd., Glasgow, UK

Bibliography

Schumann, VEB Deutscher Verlag für Grundstoffindustrie, Leipzig 1968
 Dohmke Verlag W. Giradet, Essen, 1977
 Metals Handbook, Desk Edition, ASM, Metals Park, Ohio, 44073, 1985
 Color Metallography, E. Beraha, B. Shpigler, ASM, Metals Park, Ohio, 44073, 1977
 Metallographic etching, G. Petzow, ASM, Metals Park, Ohio, 44073, 1978

Acknowledgements

We wish to thank Böhler Edelstahl GmbH, Kapfenberg, Austria, for generously supplying information, sample material, and the permission to reproduce drawing and photos on page 2 and 3, Figs. 6, 11 and 12 on page 5, photo of punching tool on page 1 and of stamping tool on page 6. Special thanks to J. Hofstätter and A. Dreindl for their co-operation.

For further details on the mentioned Struers equipment, accessories and consumables please see www.struers.com or contact your local Struers representative.

USA

Struers Inc.
 24766 Detroit Road
 Westlake, OH 44145-1598
 Phone +1 440 871 0071
 Fax +1 440 871 8188
 info@struers.com

CANADA

Struers Ltd.
 7275 West Credit Avenue
 Mississauga, Ontario L5M 5M9
 Phone +1 905-814-8855
 Fax +1 905-814-1440
 info@struers.com

SWEDEN

Struers A/S
 Smältvägen 1
 P.O. Box 11085
 SE-161 11 Bromma
 Telefon +46 (0)8 447 53 90
 Telefax +46 (0)8 447 53 99
 info@struers.dk

FRANCE

Struers S. A. S.
 370, rue du Marché Rollay
 F- 94507 Champigny
 sur Marne Cedex
 Téléphone +33 1 5509 1430
 Télécopie +33 1 5509 1449
 struers@struers.fr

NEDERLAND/BELGIE

Struers GmbH Nederland
 Electraweg 5
 NL-3144 CB Maassluis
 Tel. +31 (0) 10 599 72 09
 Fax +31 (0) 10 599 72 01
 glen.van.vught@struers.de

BELGIQUE (Wallonie)

Struers S. A. S.
 370, rue du Marché Rollay
 F- 94507 Champigny
 sur Marne Cedex
 Téléphone +33 1 5509 1430
 Télécopie +33 1 5509 1449
 struers@struers.fr

UNITED KINGDOM

Struers Ltd.
 Unit 25a
 Monkspath Business Park
 Solihull
 B90 4NZ
 Phone +44 0121 745 8200
 Fax +44 0121 733 6450
 info@struers.co.uk

IRELAND

Struers Ltd.
 Unit 25a
 Monkspath Business Park
 Solihull
 B90 4NZ
 Phone +44 (0)121 745 8200
 Fax +44 (0)121 733 6450
 info@struers.co.uk

JAPAN

Marumoto Struers K. K.
 Takara 3rd Building
 18-6, Higashi Ueno 1-chome
 Taito-ku, Tokyo 110-0015
 Phone +81 3 5688 2914
 Fax +81 3 5688 2927
 struers@struers.co.jp

CHINA

Struers Ltd.
 Office 702 Hi-Shanghai
 No. 970 Dalian Road
 Shanghai 200092, P.R. China
 Phone +86 (21) 5228 8811
 Fax +86 (21) 5228 8821
 struers.cn@struers.dk

DEUTSCHLAND

Struers GmbH
 Karl-Arnold-Strasse 13 B
 D-47877 Willich
 Telefon +49 (0)2154) 486-0
 Telefax +49 (0)2154) 486-222
 verkauf.struers@struers.de

ÖSTERREICH

Struers GmbH
 Zweigniederlassung Österreich
 Ginzkeyplatz 10
 A-5020 Salzburg
 Telefon +43 662 625 711
 Telefax +43 662 625 711 78
 stefan.lintschinger@struers.de

SCHWEIZ

Struers GmbH
 Zweigniederlassung Schweiz
 Weissenbrunnstrasse 41
 CH-8903 Birmensdorf
 Telefon +41 44 777 63 07
 Telefax +41 44 777 63 09
 rudolf.weber@struers.de

CZECH REPUBLIC

Struers GmbH
 Organizační složka
 Havlíčkova 361
 CZ-252 63 Roztoky u Prahy
 Tel: +420 233 312 625
 Fax: +420 233 312 640
 david.cernicky@struers.de

POLAND

Struers Sp. z o.o.
 Oddział w Polsce
 ul. Lirowa 27
 PL-02-387 Warszawa
 Tel. +48 22 824 52 80
 Fax +48 22 882 06 43
 grzegorz.uszynski@struers.de

HUNGARY

Struers GmbH
 Magyarországi fióktelep
 Puskás Tivadar u. 4
 H-2040 Budaörs
 Phone +36 (23) 428-742
 Fax +36 (23) 428-741
 zoltan.kiss@struers.de

SINGAPORE

Struers A/S
 627A Aljunied Road,
 #07-08 BizTech Centre
 Singapore 389842
 Phone +65 6299 2268
 Fax +65 6299 2661
 struers.sg@struers.dk

